WATER CHEMISTRY AND CORROSION - MISSING KNOWLEDGE

Otakar Jonas, P.E. Ph.D.
1113 Faun Road
Wilmington, DE 198803
Tel: (302) 478-1375 Fax: (302) 478-8173
Email: jonasinc@steamcycle.com

Abstract

This paper discusses the main water chemistry and corrosion processes and problems associated with steam generation which are not sufficiently understood. The discussion of missing knowledge is divided into four sections: 1. Root Cause and Failure Analysis, 2. Commissioning, Operation and Maintenance, 3. Water and Steam Chemistry, and 4. Corrosion.

Introduction

There have been major achievements in corrosion and water chemistry control [1 - 20] since the government initiated a study on the cost of corrosion published in 1978 by NBS (SP511-1) identified the cost of electric utility corrosion to be the highest of any U.S. industries. Ten cents of every dollar of gross production were spent on corrosion and the total cost to U.S. utilities was 9 billion dollars. This study, together with the utility recognition of the high forced outage and maintenance costs, resulted in increased R&D, formation of EPRI, and other corrective actions. In the subject area, achievable goals were formulated.

The best achievements of the corrective period (1978 to 2000), many of them through EPRI programs, but often in cooperation with other organizations [1 - 3], include:

- improved communication among designers, operators, water chemists, and researchers [1 8]
- transfer and use of knowledge
- reduction of boiler tube failures [5]
- formulation of cycle chemistry guidelines and improvement of cycle chemistry [1-3, ASME]
- better instrumentation and sampling practices [15 17]
- recognition that copper alloys should not be used [18, 19]
- better operation of condensate polishers
- better condenser tube materials and tighter condensers [4]

Remaining Problems

Besides the achievements of the previous decades, the cost of corrosion and scale is still high [21], total cost is 17.3 billion dollars per year, and efficiency and generating capacity losses due to scale and deposits persist [22 -24].

In our opinion, the main reasons for this high cost and losses are:

- unresolved cycle component design problems such as stress corrosion of turbine blade attachments and designs prone to flow-accelerated corrosion
- old uncorrected cycle design and material selection problems such as the use of copper alloy tubing in feedwater heaters and use of carbon steel in areas prone to flow-accelerated corrosion (FAC)
- equipment aging, cycling of units designed for base load
- insufficient commissioning of new units
- use of incorrect water chemistry control (some organic chemicals, phosphate hideout)
- insufficient transfer and use of existing knowledge

The lack of use of existing knowledge in cycle and component design often includes the absence of FAC and cavitation considerations, selection of wrong materials (copper alloys, high yield strength turbine disks, etc.), sampling systems with low velocity, no sampling nozzles for steam, and insufficient instrumentation. The current EPRI project on "Low-Temperature Corrosion Problems in Fossil Power Plants - State of Knowledge Report" [4] also addresses missing knowledge for major steam cycle components.

Missing Knowledge

The following tables briefly describe specific problems with knowledge of water chemistry and corrosion in the areas of root cause and failure analysis, operation and maintenance, water and steam chemistry, and corrosion. In each table, the items are in the order of priority. Discussion of selected problems follow.

Table 1

Root Cause and Failure Analysis

Problem	Missing Knowledge
Deaerator cracking	Source of stresses for corrosion fatigue, effects of welding [4, 22 - 24]
LP turbine blade	Stress amplitude, effects of mean stress, stress concentrations, pitting,
corrosion fatigue (CF)	sources of excitation, CF limits for service environments (EPRI
	BLADE) [4, 25]
Blade attachment	Effects of chemistry, crevice, galvanic, droplet charge, early
stress corrosion	condensate [4, 11]
cracking (SCC)	
L-0R blade failures	Effect of trailing edge erosion [4, 22]
Turbine SCC and CF	Effects of heater box and periodic overspeed, LCCF (low cycle
	corrosion fatigue)
Flow-accelerated	Effects of organic water treatment chemicals and their decomposition
corrosion	products [4, 22, 23]
CF of boiler tubes	Effect of high pH, NaOH [5]
Hydrogen damage	Effects of NaOH, acid phosphate [5, 26]
Boiler tube corrosion	Effects of "acid phosphates", maracite [5, 26, 27]
Water droplet erosion	Predictive equations, effects of chemistry [7, 28]
Corrosion in steam	Local, at surface environments [1, 2, 5, 7 - 14]
and water	
Forced-circulation	Mechanism
boiler orifice plugging	

Table 2

Commissioning, Operation and Maintenance

Problem	Missing Knowledge
Boiler carry-over	How to measure for AVT and EP (equilibrium phosphate)
Pre-operational chemical cleaning	When needed? Citric acid vs. high Cr steels in superheaters
Steam and air blows	Blow parameters for efficient blows, better monitoring [29]
Disposal of EDTA	How to dispose of used solutions, reduce cost
Oxide scale and deposits in	How to clean
feedwater systems of older fossil	
and nuclear units	
Removal of preservatives	Need, procedures
SF ₆ for leak detection	Environmental impact
Sample tubing deposits	How to clean, criteria

Table 3
Water and Steam Chemistry

Problem	Missing Knowledge
Boiler carry-over	Effect of NaOH, EPT, EDTA, dispersants, suspended solids, organic
	acids
Turbine steam chemistry	Early condensate and liquid films in PWRs [7 - 14]
Steam chemistry	Hydrolysis of salts including sodium phosphate
Impurity concentration	Chemistry, reaction with oxides, hideout, pH, concentration for
in boiler tubes	AVT, EPT
Confusion with EPT	Is there acid phosphate corrosion during phosphate hideout? How
	can solid maracite, NaFePO ₄ be corrosive? Nuances of opinions.
Boiler tube scale growth	Effects of water chemistry
Scale growth in liquid	Effects of flow, surface finish, mixed oxides, suspended solids
water	
At-temperature and on-	Is it ready after 20 years of research?
surface pH measurement	
Organics vs.	Long-term effects of discharges on aqueous systems [20]
environment	
Organic water treatment	Decomposition products, their transport around the cycle, carry-
chemicals	over, deposits, corrosion effects, surface reactions [20]
Hydrazine vs. substitutes	True environmental impact, effects of organic decomposition
	products [20]
Volatility	Basic model [30]
Condensation	Homogeneous or heterogeneous, nucleation seeds, Wilson line,
	electrical charges, effect of chemistry [12 - 14]

Table 4

Corrosion

Problem	Missing Knowledge
Corrosion data	Accessible pertinent corrosion, SCC, CF, pitting,
	crevice, and galvanic data
Design against SCC and CF	Design rules, allowable stresses, defects, interaction of
	SCC and CF, variable amplitude CF and fatigue [31]
SCC in PWR LP turbines	Steam and surface chemistry (amines, organic acids
	and salts, boric acid) [32]
Boiler tube corrosion vs. hideout	Corrosion data for maracite, direct measurement of
	acid phosphate corrosion (corrosion hydrogen) [26]
Boiler tube corrosion fatigue	Crack initiation and growth rate data for sodium
	phosphate, NaOH, EDTA, polymers [5]
Cavitation	Effects of water chemistry
Stress corrosion cracking	Crack initiation data for pertinent aqueous and steam
	environments
Corrosion of bolts, disk steeples	Effects of Loctite, graphite, etc.
Galvanic series	For steam cycle environments
Stress corrosion and corrosion fatigue	Basic mechanisms (see Epilogue) [33 - 37]
Turbine SCC and CF	Effects of droplet charges

Examples

Deaerator Cracking [24]

Stress corrosion and corrosion fatigue cracking of deaerator welds has been a major problem for several decades. It is also a safety issue because it has resulted in fatalities. Thirty to forty percent of inspected deaerators are found to have cracks and, depending on the local regulations, every indication may have to be repaired.

Root causes of this problem have not been identified and the only correlation found was that of the apparent crack propagation rate and the age of the deaerator (see Figure 1). While several deaerator users measured stresses, the source of alternating stresses causing corrosion fatigue has not been found. The only source of high-cycle stresses reported in literature is called "water piston" which can occur in horizontal vessels with a water level as an instability which depends on the storage tank geometry, viscosity, and location of the water level (see Figure 2).

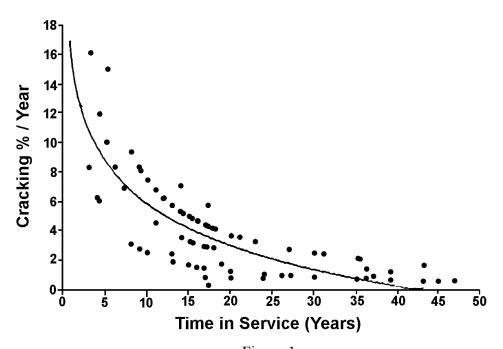


Figure 1
Deaerator Storage Tank Weld Cracking: % of Wall Thickness per Year vs. Time in Service

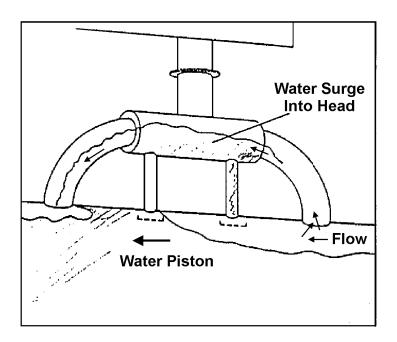


Figure 2 Water Piston

Steam and Air Blow

These costly pre-commissioning procedures are an art which is solely based on experience. An online monitoring of a steam blow [29] indicates that there could be extended periods of time wasted when there is no removal of impurities from the steam piping and that certain steam blow conditions, such as the length of the blows, are more effective than others (Figure 3). The most common, infrequent monitoring is with impact targets which does not allow for timely blow condition adjustment. Similar situations exist for air blows.

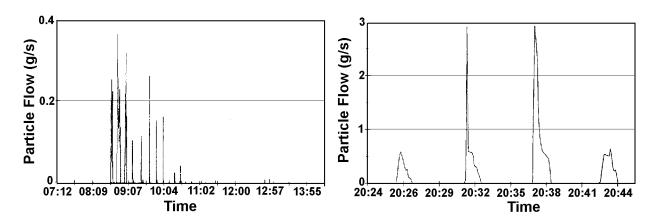


Figure 3
Steam Blows vs. Removal of Particulate Matter

Impurity Concentration on Boiler Tubes

It is assumed that soluble impurities such as NaOH and NaCl concentrate at the hot tube surfaces in the liquid because of the temperature gradient - vapor pressure of the solution, thermodynamic relationships. The second impurity concentration speculative model is the "wick boiling" model for the surface oxide. While these models may reflect reality, they have never been experimentally confirmed and the effects of boiling, water treatment, flow, and solid phases have not been determined.

Confusion with Equilibrium Phosphate Treatment - EPT [26, 27]

The concepts of not exceeding the equilibrium (acceptable) concentration of sodium phosphate in boiler water and of increasing pH at low phosphate concentrations required for high pressure high and heat flux boilers with low concentrations of NaOH are sound. However, the speculative conclusions on corrosion by NaFePO₄ (a solid under boiler conditions) need to be experimentally evaluated. In the international survey [3], several participants reported phosphate hideout and pH swings without any tube corrosion consequences. It should also be emphasized that for EPT, the limits of corrosive impurities in the boiler water are as low as those for AVT and that, for many applications, condensate polishing may be required.

Carry-over of a Dispersant and Turbine MW Loss

There have been multiple cases of polymeric dispersant carry-over from the boiler water into the turbine and a consequent buildup of hard organic deposits in turbine control valves and on turbine blades. In one case, the deposit prevented valve closure, resulting in a turbine wreck due to overspeed. Figure 4 shows heavy deposits on turbine blades caused by carry-over of a polymeric dispersant, which resulted in loss of MW and overloading of the thrust bearing.



Figure 4
Turbine Deposits Caused by Carry-over of a Polymeric Dispersant

Conclusions and Recommendations

- 1. A significant amount of knowledge is not available, costing the steam generation industry millions of dollars annually. Included is the knowledge needed to solve some of the costliest generic corrosion problems, such as deaerator cracking and steam turbine blade attachment SCC.
- 2. Application of existing knowledge needs to be improved and better used in root cause analysis and problem solving. With the current staffing at utility and industrial companies, the transfer and application of the existing knowledge is often provided by consultants. This is OK as long as the management of the owners/operator companies is aware that this knowledge exists.
- 3. The best application of existing knowledge is in the cycle and component design phase. However, design reviews of water chemistry and corrosion are still rare (FAC, SCC and CF in turbines, etc.)

Epilogue

On Stress Corrosion - S. P. Rideout (Savannah River Laboratory), 1969 [33]

The image of stress corrosion I see Is that of a huge unwanted tree, Against whose trunk we chop and chop, But which outgrows the chips that drop;

And from each gash made in its bark A new branch grows to make more dark The shade of ignorance around its base, Where scientists toil with puzzled face.

Chemists and metallographers, Technicians and philosophers, Though struggling individually, Their common goal: to fell the tree.

At intervals researchers gather, And on mechanisms all palaver; Each to his own work will refer, Ignoring those who don't concur, But as we speculate and ponder, Those who run the mills out yonder To us with anxious voices wail, "Please help us lengthen 'time to fail!'

For us to pay your research bills By sale of products from our mills, Wheels must turn and planes must fly, And on high-strength alloys we rely."

Thus, as we argue with each other, Let us not forget our brother Our Siamese twin, the engineer, Whose working profits sent us here.

The Conference ended, let us pledge To go again with sharpened edge, And with redoubled energy To pit ourselves against this tree.

References

- 1. ASME Handbook on Water Technology for Thermal Power Systems. ASME, 1989.
- 2. Interim Consensus Guidelines on Fossil Plant Cycle Chemistry. EPRI, Palo Alto, CA, June 1986. CS-4629.
- 3. O. Jonas and R. Dooley. "International Water Treatment Practices and Experience." Paper No. IWC-90-41. *International Water Conference*. Pittsburgh, PA. 1990.
- 4. Low-Temperature Corrosion Problems in Fossil Power Plants State of Knowledge Report. EPRI. Palo Alto, CA: To be Published 2003.
- 5. B. Dooley and W. McNaughton. *Boiler Tube Failures: Theory and Practice*. EPRI. Palo Alto, CA: 1996.
- 6. Flow-Accelerated Corrosion in Power Plants. EPRI, Palo Alto, CA. 1996. TR-106611.
- 7. Steam Turbine Efficiency and Corrosion: Effects of Surface Finish, Deposits, and Moisture. EPRI. Palo Alto, CA. October 2001. Report 1003997.
- 8. O. Jonas. "Understanding Steam-Cycle Chemistry." *Power*. September-October 2000.
- 9. O. Jonas and R.B. Dooley. "Impurity Concentration Processes in Steam Turbines." 3rd Intl. VBG/EPRI Conference on Steam Chemistry, Freiburg, Germany. June 22-25-1999.
- 10. O. Jonas and N. Rieger. *Turbine Steam Chemistry and Corrosion*. EPRI. Palo Alto, CA: Feb. 1994. TR-103738.
- 11. O. Jonas, B. Dooley, and N. Rieger. "Steam Chemistry and Turbine Corrosion State-of-Knowledge." Paper IWC-93-51. 54th International Water Conference, Pittsburgh, PA. 1993.

- 12. O. Jonas. "Effects of Steam Chemistry on Moisture Nucleation." *Moisture Nucleation in Steam Turbines*. EPRI. Palo Alto, October 1997. TR-108942.
- 13. O. Jonas. "Condensation in Steam Turbines New Theory and Data." *ASME IJPGC 98*, Baltimore, August 23-26, 1998.
- 14. M. Stastny, O. Jonas, et al. "Behaviour of Chemicals in the Steam Flow through Phase Transition Zone of Turbines and its Mathematical Modeling." *Skoda Review*. January 1998.
- 15. Guideline Manual on Instrumentation and Control for Fossil Plant Cycle Chemistry. Electric Power Research Institute, Palo Alto, CA, April 1987. CS-5164.
- 16. O. Jonas. *Development of a Steam Sampling System*. EPRI, Palo Alto, CA, Dec. 1991. TR-100196.
- 17. O. Jonas. "On-Line Diagnosis of Turbine Deposits and First Condensate," 55th Annual Intl Water Conf., Pittsburgh, PA, 1994.
- 18. State-of-Knowledge of Copper in Fossil Plant Cycles. EPRI. Palo Alto, CA: Sept. 1997. TR-1086460.
- 19. O. Jonas, et al. "Copper Deposition and MW Loss Problem Solutions." 57th International Water Conference. Pittsburgh, PA. October 1996.
- 20. O. Jonas. "Use of Organic Water Treatment Chemicals." *VGB Conference*. Organische Konditionierungs-und Sauerstoffbindemittel, Lahnstein, Germany. March 1994.
- 21. Cost of Corrosion in the Electric Power Industry. EPRI. Palo Alto, CA: 2001. 1004662.
- 22. O. Jonas. "Safety Issues in Fossil Utility and Ind'l Steam Systems." Mat'ls Perf. May 2001.
- 23. O. Jonas. "Corrosion and Water Chemistry Problems in Steam Systems Root Causes and Solutions." *Materials Performance*. December 2001.
- 24. O. Jonas. "Deaerators: An Overview of Design, Operation, Experience and R&D." *Proceedings of the American Power Conference*, Vol. 49, A979. 1987.
- 25. BLADE-STTM Version 3. Available from STI Technologies, Rochester, NY. February 2000.
- 26. J. Stodola. "Fifteen Years of Equilibrium Phosphate Treatment (Correct Use of Phosphates in Drum Boilers.)" *Power Plant Chemistry*, 5(2), 2003.
- 27. O. Jonas and K. Layton. "Phosphate Boiler Water Treatment For High Pressure Boilers." *Proc. 2nd Fossil Plant Cycle Chemistry Conf.* EPRI, Palo Alto, CA: January 1989. GS-6166.
- 28. F.J. Heymann. "Toward Quantitative Prediction of Liquid Impact Erosion." *ASTM STP 474*, American Society for Testing and Materials, 1970.
- 29. O. Jonas. "Monitoring of Superheater and Reheater Exfoliation and Steam Blow. *International Water Conference*. Pittsburgh, PA. 1995.
- 30. Assessment of the Ray Diagram. EPRI. Palo Alto, CA: August 1996. TR-106017.
- 31. O. Jonas. "Design Against Localized Corrosion. "Second Int'l Symp. on Env. Degradation of Mat'ls in Nuclear Power Systems-Water Reactors." Monterey, CA. Sept. 1985.
- 32. EPRI Project: SONGS LP Turbine Environment. EPRI. Palo Alto, CA: To Be Published.
- 33. Proc. of Conference Fundamental Aspects of Stress Corrosion Cracking. NACE, 1969.
- 34. F. Ford. *Mechanisms of Environmental Cracking in Systems Peculiar to the Power Generation Industry*. EPRI. Palo Alto, CA. September 1982. NP-2589.
- 35. D. Vermilya. "Reaction Films, Metal Dissolution and Stress Corrosion Cracking." *Proc. of Conference Fundamental Aspects of Stress Corrosion Cracking*. NACE, 1969.
- 36. H. Uhlig. "An Evaluation of Stress Corrosion Cracking Mechanisms." *Proceedings of Conference Fundamental Aspects of Stress Corrosion Cracking*. NACE, 1969.
- 37. O. Jonas. "Molecular Modeling of Corrosive Environments in Cracks." *Effects of the Environment on the Initiation of Crack Growth*. ASTM STP 1298. ASTM, 1997.